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(54) Device for mapping corneal topography.

(57) A device for mapping the topography of the cornea (38) of an eye has a light source (10) for directing a beam of collimated monochromatic light characterized by a flat wave front onto the cornea. Positioned between the light source and the cornea is an objective lens (32) for focusing this flat wave front toward the cornea as a converging spherical wave front. The light reflected from the cornea

passes back through the objective lens to establish a reflected wave front having deviations from the flat wave front caused by aberrations on the cornea that are indicative of corneal topography. This reflected wave front is then segmentally focused by a lens array (64) into a pattern which reveals the deviations for use in mapping the topography of the cornea.

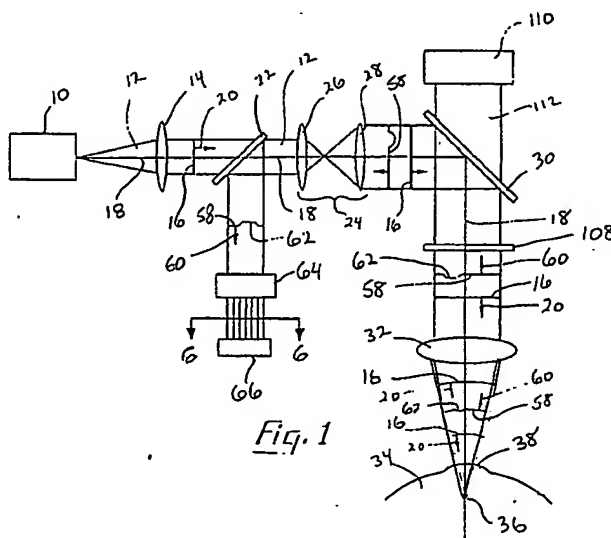


Fig. 1

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FIELD OF THE INVENTION

The present invention pertains generally to ophthalmic instruments. More particularly, the present invention pertains to ophthalmic instruments which measure and determine the corneal topography of a human eye. The present invention is particularly, but not exclusively, useful for homogeneously mapping the topography of the entire cornea of the eye with equal precision and uniform accuracy.

BACKGROUND OF THE INVENTION

Due to the enhanced precision with which ophthalmic surgery can now be performed using laser instruments, it is increasingly important that corneal topography be determined with an accuracy which will allow full exploitation of the capabilities and potential of these instruments. Further, it is important and desirable that the entire anterior surface area of the cornea, and not just a part thereof, be accurately mapped in order for laser instruments to be employed most efficaciously. To this end, several devices have been proposed.

One type of instrument which is now used to measure the anterior surface of the cornea relies on the use of Placido disc illumination. In accordance with the technique used by such an instrument, a template having a series of expanding planar concentric circles, or rings, is positioned in front of the eye and the light reflected from the cornea through the template is analyzed. Specifically, the distortion of light reflected through the ring pattern by the conditions that exist on the corneal surface is analyzed to help determine the corneal topography. As can be expected, the efficacy of this technique is dependent on the precise geometric placement of the ring pattern with respect to the corneal reflections. Importantly, however, the accuracy of this technique is greatly diminished, indeed obviated, as the diameter of the ring is diminished. Unfortunately, this occurs in the center of the template which receives light reflected from the center of the cornea. Thus, the diminution in accuracy occurs at the very part of the cornea where the greatest accuracy is required.

Another type of device for analyzing a corneal contour employs a modal wave front estimation from phase derivative measurements. An example of such a device is disclosed and discussed in an article written by Philip C. Baker entitled "Holographic Contour Analysis of the Cornea" which appeared in SPIE Vol 1161 (1989). In the operation of this device, a wave front reflected from the corneal surface is detected and analyzed to determine phase change interferences which result from perturbations on the surface. An interference

fringe pattern is thus created with data which can be digitized for evaluation. There are, however, some disadvantages with such a device. For example, the return signal is extremely noisy. Thus, there is a high probability for random reconstruction error. Further, the technique involves numerical complexities and an inherent problem for determining compatible polynomials. Still further, and perhaps most importantly, phase derivative measurements require analysis of an unperturbed reflected wave front. Stated differently, the signal to be analyzed is spread over the whole wave front. Consequently, in order to obtain a signal which will yield a fringe pattern with sufficient information to be meaningfully analyzed, the light source used must provide a relatively high intensity input, i.e. a flash of light. This, at best, can be uncomfortable for the patient.

In light of the above, an object of the present invention is to provide a device for mapping the topography of the eye which provides a uniform homogeneous mapping of the entire corneal surface of most significant interest. Another object of the present invention is to provide a device for mapping the topography of the eye which is equally accurate for all portions of the anterior surface of the cornea which are of significant interest. Still another object of the present invention is to provide a device for mapping the topography of the eye which gives information that can be beneficially used for a wide variety of ophthalmic procedures. Yet another object of the present invention is to provide a device for mapping the topography of the eye which is relatively easy to use and comparatively cost-effective.

SUMMARY OF THE INVENTION

In one aspect, the invention provides a device for mapping the topography of an object characterised in that it comprises:

means for generating a beam of collimated monochromatic light having a directed wave front of predetermined curvature;

means for directing said beam toward said object;

means for receiving light of said beam reflected by said object, said reflected light having a reflected wave front indicative of said topography; and

means for segmentally focusing said reflected wave front to detect deviations of said reflected wave front from said directed wave front to map said topography.

The preferred embodiment of the device for mapping the topography of the cornea of the eye includes a light source for generating a beam of collimated monochromatic light. As intended for the

present invention, the beam of light from the light source is characterized by a directed wave front having a predetermined curvature. Preferably, this predetermined curvature is such that the directed wave front is flat. An objective lens is positioned on the optical axis which extends from the light source to the surface of the cornea and this lens is used to focus the directed wave front toward the surface of the cornea. As so focused by the objective lens, the beam of light travels toward the cornea with a converging spherical wave front.

Light in the beam that is reflected from the surface of the cornea passes back substantially along the optical axis and through the objective lens. After reflection from the cornea, the reflected light establishes a reflected wave front which differs from the initially directed wave front by deviations which are indicative of corneal topography. A beam splitter is positioned on the optical axis between the light source and the objective lens for directing the reflected wave front toward a detector.

The device of the present invention has a detector which includes a lens array for separately focusing segments of the reflected wave front, and a charge-coupled device for determining the location of the focal points of the focused segments. More specifically, the lens array comprises a first lens layer having a plurality of juxtaposed cylindrical lenses which are positioned adjacent a second lens layer having a plurality of juxtaposed cylindrical lenses. As positioned, the longitudinal axes of the lenses of the first layer are substantially perpendicular to the longitudinal axes of the lenses of the second layer. Consequently, the light characterized by the reflected wave which is incident on the lens array is concentrated by separately focusing segments of the reflected wave which are substantially defined by the diameters of the cylindrical lenses. These individually focused segments of the reflected wave front are then incident on the charge-coupled device and the location of incidence of their focal points on the charge-coupled device is used in mapping the corneal topography.

In the operation of the device for mapping the cornea of the eye, it is to be understood that the detector would focus segments of a light beam having a flat wave front into a grid or pattern of aligned focal points. Thus, if the area of the cornea being mapped is perfectly spherical, the reflected wave front will be flat and this aligned grid pattern will result. On the other hand, a reflected wave front passing through the lens array, which is not a flat wave front, will have deviations that cause movement or misalignment of the segment focal points. The charge-coupled device is used to determine the actual pattern of segment points, including misalignments, and present this pattern for use in subsequent calculations to map the corneal

topography.

In an alternate embodiment of the present invention, the beam splitter is replaced by a polarized beam splitter and a quarter wave plate is added. Specifically, monochromatic polarized light is directed along the optical axis through the polarized beam splitter and is then rotated by the quarter wave plate enroute to the cornea. The light reflected from the cornea is then again rotated by the quarter wave plate to be polarized perpendicular to the incoming wave, and is subsequently diverted off the optical axis and toward the detector by the polarized beam splitter.

For purposes of the present invention, the light source is preferably a combination of a laser diode and a collimating lens. The light source may, however, be a combination of a collimating lens and an incandescent light source with a spectral filter which is positioned relative to the incandescent source to pass monochromatic light toward the cornea.

The novel features of this invention, as well as the invention itself, both as to its structure and its operation, will be best understood from the accompanying drawings, taken in conjunction with the accompanying description, in which similar reference characters refer to similar parts, and in which:

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic diagram of the interactive components of the device of the present invention shown in relation to the eye and cornea of a patient;

Figure 2 is a cross-sectional schematic showing incident and reflected light relative to the cornea of an eye;

Figure 3 is a perspective view of the lens array of the present invention with portions broken away for clarity;

Figure 4 is a cross-sectional view of a portion of the lens array as seen along the line 4-4 in Figure 3 in its relationship to both an input reflected wave front and a charge-coupled device;

Figure 5 is a cross-sectional view of a portion of the lens array as seen along the line 5-5 in Figure 3 in its relationship to both an input reflected wave front and a charge-coupled device;

Figure 6A is a grid pattern of segment focal points as detected by the device of the present invention that is indicative of a perfectly spherical cornea; and

Figure 6B is a grid pattern of segment focal points as detected by the device of the present invention that is indicative of an aberration on the cornea.

DESCRIPTION OF THE PREFERRED EMBODI-

MENT

Referring initially to Figure 1, it will be seen that the device for mapping corneal topography according to the present invention includes a light source 10. Importantly, light source 10 generates a beam 12 of monochromatic light which is collimated by a collimating lens 14. Preferably, light source 10 is a laser diode of any type well known in the pertinent art. For example, a laser diode which emits light having a 820 nm wavelength is suitable for the present invention. Light source 10 may, however, be an incandescent lamp having a spectral filter. In either case, it is necessary that light source 10, in combination with collimating lens 14, generates a coherent beam 12 of monochromatic light.

As will be appreciated by the skilled artisan, the beam 12 of collimated monochromatic light that is generated by light source 10 will be characterized by a directed wave front 16 which is flat and which travels along the optical axis 18 of the device in a direction indicated by the arrow 20. Although the predetermined curvature for directed wave front 16 is preferably flat, modifications of the device are possible to accommodate directed wave fronts 16 having a different predetermined curvature. It is important, however, that directed wave front 16 have a predetermined curvature.

A 50/50 beam splitter 22, of any type well known in the pertinent art, is positioned on optical axis 18 to pass beam 12 toward a telescopic unit 24. As shown in Figure 1, telescopic unit 24 includes a pair of lenses 26, 28 which are optically arranged in a well known configuration to expand beam 12 as it progresses along optical axis 18 in the direction of arrow 20. Another 50/50 beam splitter 30 is positioned on optical axis 18 to divert the beam 12, and consequently directed wave front 16, toward an objective lens 32.

In accordance with the present invention, objective lens 32 is positioned relative to the eye 34 to focus the beam 12 onto the center of curvature 36 of the cornea 38. Thus, the directed wave 16 emerges from objective lens 32 and travels toward the center of curvature 36 of cornea 38 as a converging spherical wave front. As an order of magnitude, the radius of curvature (i.e. the distance from the center of curvature 36 to the anterior surface of cornea 38) will be approximately seven and eight tenths millimeters (7.8 mm). It is a substantially accurate assumption that, for a normal eye 34, the center of the cornea 38 (e.g. a circular area of approximately four millimeters (4 mm) in diameter) is spherical in its contour. Accordingly, for a spherical-shaped cornea 38, all the light rays of wave front 16 will impact cornea 38 simultaneously and be reflected back along the same

path.

A more complete appreciation of the optics involved may be had by reference to Figure 2. With reference to Figure 2, first consider a surface portion 40 of cornea 38 that is spherically contoured. Because the directed wave front 16 after being focused by objective lens 32 is now also spherical, a light ray 42 in wave front 16 will travel in a direction that is normal to surface portion 40 of cornea 38. Thus, as light ray 42 approaches portion 40 in the direction indicated by arrow 20, it will be reflected back along the same path in the direction of arrow 44. Again, this occurs when the converging spherical wave front 16 is incident on a spherical surface portion 40 of eye 34.

It happens, however, that cornea 38 may be aspherical and have aberrations such as the indentation 46. To understand how an indentation 46 will affect directed wave front 16, consider the light ray 48 of wave front 16 which is incident on cornea 38 in the area of indentation 46. At the point 50 where light ray 48 strikes cornea 38 it will be seen that the direction normal to cornea 38 is represented by the line 52. As is well known to the skilled artisan, the angle of incidence for a light ray, as measured from normal, equals the angle of reflection, as measured from this same normal. Consequently, as light ray 48 of directed wave front 16 strikes point 50 on cornea 38 at an angle of incidence 54, the light ray 48 will be reflected from cornea 38 at an angle of reflection 56 that is equal to the angle of incidence 54. In order to appreciate the orders of magnitude involved, it is known that a six (6) diopter indentation 46 in cornea 38 will cause a light ray 48 to reflect from cornea 38 through an angle of approximately fifteen (15) arc minutes. Thus, in such a case, both the angle of incidence 54 and the angle of reflection 56 will be approximately equal to seven and one half (7.5) arc minutes. In any event, all of the light rays in directed wave front 16, including both the normal and angled rays, are reflected from cornea 38 as a reflected wave front 58.

As shown in Figure 1, after the directed wave front 16 is incident on cornea 38, it returns as a reflected wave front 58 which travels back along the optical axis 18 in the direction indicated by arrow 60. Further, for purposes of discussion, reflected wave front 58 is shown with a deviation 62 which is indicative of a topographical aberration (e.g. indentation 46) on the anterior surface of cornea 38. More specifically, deviation 62 is shown on the reflected wave front 58 before and after it passes through objective lens 32.

In Figure 1, it can be seen that the reflected wave front 58 is reflected by beam splitter 30 back through the telescopic unit 24 and is then diverted off optical axis 18 by the beam splitter 22. The

diverted reflected wave front 58 is then incident on a detector which includes a lens array 64 and a charge-coupled device (CCD) 66. Specifically, light incident on lens array 64 is concentrated in segments and focused by lens array 64 onto the CCD 66.

Figure 3 shows that the lens array 64 comprises a first or upper lens layer 68 which is positioned adjacent a second or lower lens layer 70. More specifically, lens layer 68 comprises a plurality of juxtaposed cylindrical lenses 72. Similarly, lens layer 70 comprises a plurality of juxtaposed cylindrical lenses 74. As shown, the cylindrical lenses 72 of lens layer 68 are positioned with their respective longitudinal axes aligned in the indicated x-direction. On the other hand, the cylindrical lenses 74 of lens layer 70 are positioned at right angles to the lenses 72 and have their respective longitudinal axes aligned in the indicated y-direction.

The effect lens array 64 has on a reflected wave front 58 can best be seen in Figures 4 and 5 where it will be seen that the reflected wave front 58, including deviation 62, is characterized by various combinations of both flat portions 76 and angled portions 78. First consider the flat portion 76 of reflected wave front 58 as shown in Figure 4. As light rays in this portion 76 pass through the cylindrical lens 72a they converge toward a theoretical focal line (not shown) that is parallel to the longitudinal axis of the lens 72a. They do not, however, converge along the longitudinal axis of the lens 72a. As these same rays then pass through the cylindrical lens 74a they are focused to converge on a focal line (not shown) that is theoretically perpendicular to the focal line of lens 72a. The result of the combined focusing of lenses 72a and 74a is that the light rays in flat portion 76 are focused to a focal point 80 which is at the intersection of the theoretical focal lines and located on surface 82 of CCD 66. In contrast, consider the effect lens array 64 has on the angled portion 78 of reflected wave front 58. While lens 72a still focuses the light to converge on a theoretical focal line that is parallel to the longitudinal axis of lens 72a, by virtue of the inclination of angled portion 78 this light is shifted along the longitudinal axis of the lens 72a. As this light next passes through cylindrical lens 74b it is focused, as before with flat portion 76, onto a theoretical line that is parallel to the longitudinal axis of lens 74b. Again, the result of the combined focusing of lens 72a and 74b is a focal point. In this case, however, the light in angled portion 78 is focused to a focal point 84 that is shifted a distance Δx_1 from the point 86 where light in angled portion 78 would have been focused had portion 78 been flat.

Under an analysis similar to the one used

above for flat portion 76 and angled portion 78, it can be appreciated that the light in angled portion 88 shown in Figure 4 will be focused by cylindrical lens 72a and cylindrical lens 74c onto a focal point 90 that is a distance Δx_2 from the point 92 where light in angled portion 88 would have been focused had portion 88 been flat.

The effect lens array 64 has on reflected wave front 58 in the y-direction can be best seen by referring to Figure 5. Again, as along the x-direction, reflected wave front 58 can be characterized by various combinations of both flat portions 94 and angled portions 96. Using the same analysis as above, the light in flat portion 94 which passes through cylindrical lenses 72c and 74a will be focused to an unshifted focal point. On the other hand, light in angled portion 96 is shifted through a distance Δy and focused to the focal point 100 which is at the distance Δy from the point 102 where it would otherwise have been focused had portion 96 been flat.

With the above in mind, it is to be appreciated that when each cylindrical lens 72, 74 has a diameter d , the reflected wave front 58 will be effectively divided into contiguous square segments which have sides of length d . As intended for the present invention each of the lens layers 68, 70 respectively comprise eleven (11) cylindrical lenses 72, 74. Further, each cylindrical lens 72, 74 is preferably one (1) mm in diameter (i.e. d equals one (1) mm). Consequently, lens array 64 individually focuses reflected wave front 58 into one hundred twenty-one (121) separate segments which are each one (1) mm square. Thus, the light in reflected wave front 58 is concentrated by lens array 64 in each segment and focused onto surface 82 of CCD 66. For purposes of the present invention, lens array 64 is optically positioned sufficiently near cornea 38 so that the light rays in each segment of reflected wave front 58 were initially in a respectively corresponding segment of directed wave front 16. This will effectively be the case for all light rays, to include even those which are reflected at an angle from cornea 38. This is so because the reflected angle is usually less than fifteen (15) arc minutes when light is reflected from cornea 38 as a result of a corneal aberration such as indentation 46.

Figures 6A and 6B are representative of the locations of focal points on surface 82 of CCD 66 that result from the passage of reflected wave front 58 through lens array 64. Specifically, Figure 6A shows a grid or pattern of aligned focal points 80 which would result if reflected wave front 58 were flat. This would be the case if cornea 38 is spherical. Figure 6B, on the other hand, illustrates a case where reflected wave front 58 includes deviations due to an indentation 46 on cornea 38. Specifically,

Figure 6B shows a representative focal point 104 which has been moved through the distances Δx and Δy because of an indentation 46 on cornea 38. Although the deviation 62 discussed herein has used indentation 46 as an example, it is to be appreciated that cornea 38 may have bumps (not shown) as well as indentations on its surface. Whether the surface aberration is a bump or an indentation does not, however, make any difference in the functioning of the device for mapping corneal topography according to the present invention. In either case, the same basic principles of optical physics are employed.

As will be appreciated by the skilled artisan, surface 82 of CCD 66 may comprise a plethora of pixels (not shown) which are responsive to the increased intensity of light at the various focal points on surface 82. With electronic componentry (not shown) these focal points can be oriented in their relationship to each other and the deviations from a predetermined pattern used to map the topography of cornea 38. Further, using appropriate mathematical computations (e.g. Taylor Series) the topographical surface of cornea 38 between the various focal points can be approximated with sufficient accuracy. More specifically, the skilled mathematician will appreciate that, with the proper calculation of appropriate polynomials, an algorithm can be constructed for computation of an approximated surface for cornea 38. Stated differently, and somewhat simplistically, an algorithm can be formulated by one skilled in the pertinent art to convert the information developed by CCD 66 (e.g. the pattern of points 102 as shown in Figure 6B) into an approximate model of the corneal topography (e.g. the surface portion 40 shown in Figure 2).

By way of example, Figure 6A shows an aligned grid of focal points which are representative of a spherical cornea 38. An indentation (e.g. indentation 46) in cornea 38, however, will cause the reflected wave front 58 to create a pattern of focal points such as the one shown in Figure 6B. If so, the various deviations, Δx and Δy , of each focal point 104 can be used to map corneal topography.

Calibration of the device for mapping corneal topography can be accomplished by initially diverting a directed wave front 16 through lens array 64 without having it reflected by cornea 38. Thus, a base pattern, such as shown in Figure 6A, can be created with which to compare an actual pattern such as the one shown in Figure 6B which is reflected from cornea 38.

In an alternative embodiment of the device for mapping the topography of the cornea, as stated above, the light source 10 may be an incandescent light rather than a laser diode. If an incandescent light is used, however, a spectral filter will be required to establish a beam 12 of monochromatic

light. In either event, a collimating lens 14 must be employed to ensure that the light rays in beam 12 are collimated.

It is also possible to incorporate beam splitter 22 as a polarized beam splitter. If so incorporated, a quarter wave plate 108 must be positioned on optical axis 18 somewhere between the polarized beam splitter 22 and cornea 38. Preferably, quarter wave plate 108 is positioned between beam splitter 30 and objective lens 32 as shown in Figure 1. As so positioned, quarter wave plate 108 will effectively rotate the light in beam 12 in a manner well known to the skilled artisan so that reflected wave front 58 is diverted off optical axis 18 and toward lens array 64 by the polarized beam splitter 22.

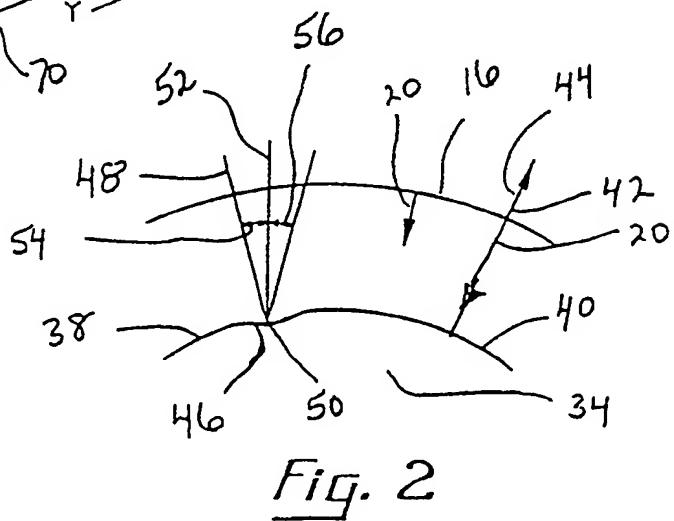
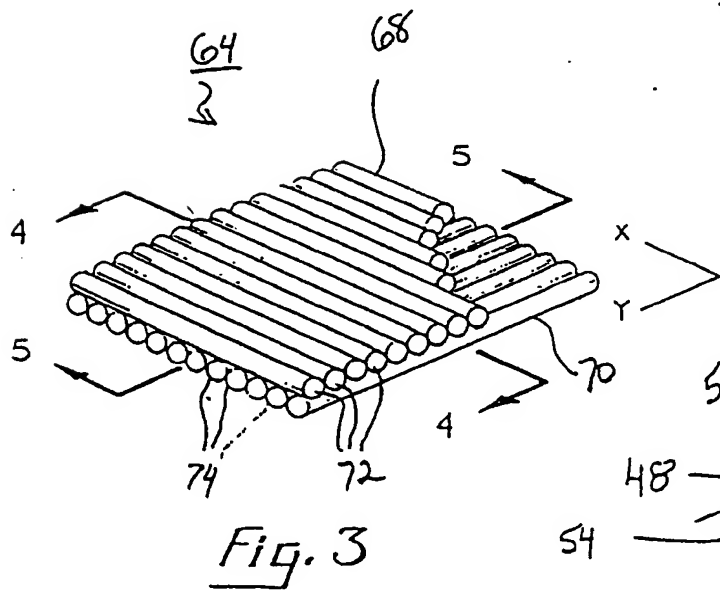
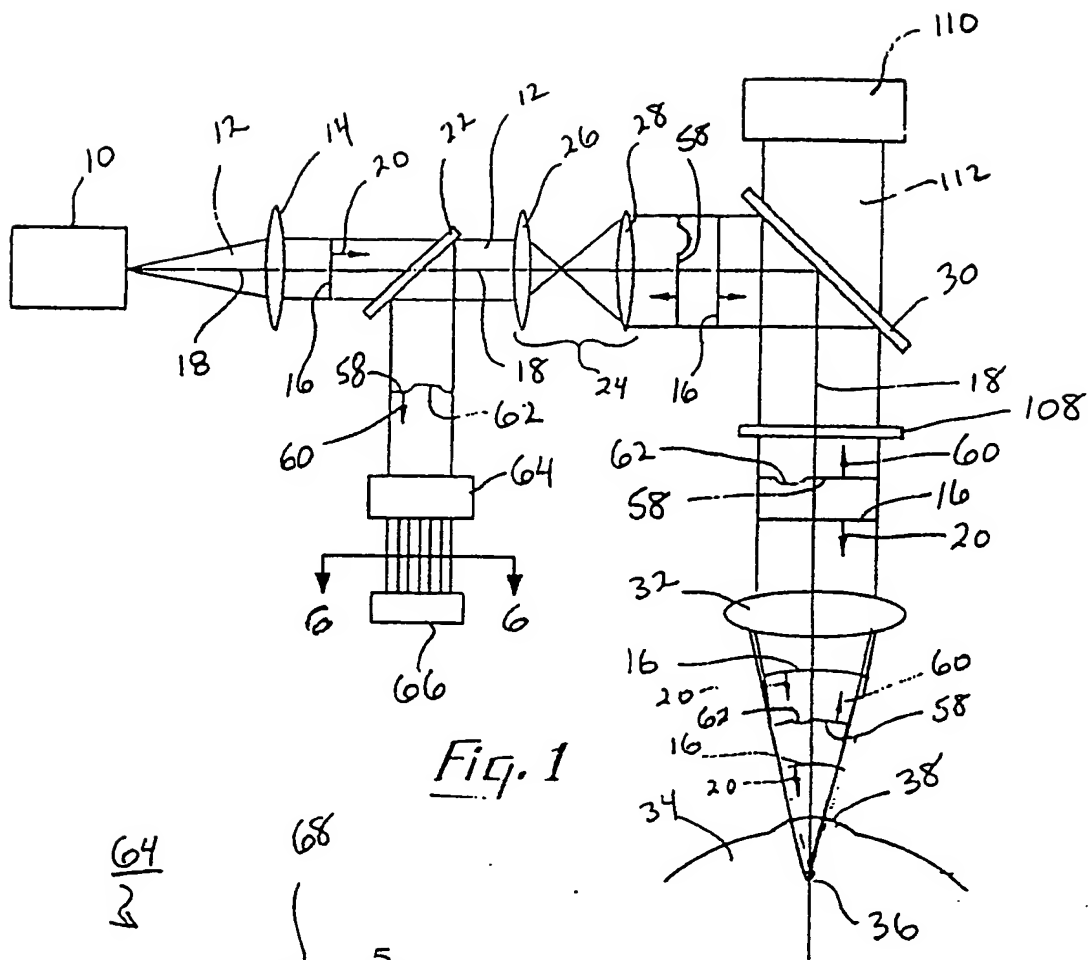
As can be appreciated by reference to Figure 1, the device of the present invention is adaptable for use with a surgical laser system 110. Specifically, a surgical laser system 110 can be optically positioned relative to beam splitter 30 to direct a laser cutting beam 112 toward cornea 38, in a manner well known in the art, for the purpose of performing ophthalmic surgery.

While the particular device for mapping corneal topography as herein shown and disclosed in detail is fully capable of obtaining the objects and providing the advantages herein before stated, it is to be understood that it is merely illustrative of the presently preferred embodiments of the invention and that no limitations are intended to the details of construction or design herein shown other than as defined in the appended claims.

Claims

1. A device for mapping the topography of an object characterised in that it comprises:
 - means for generating a beam of collimated monochromatic light having a directed wave front of predetermined curvature;
 - means for directing said beam toward said object;
 - means for receiving light of said beam reflected by said object, said reflected light having a reflected wave front indicative of said topography; and
 - means for segmentally focusing said reflected wave front to detect deviations of said reflected wave front from said directed wave front to map said topography.
2. A device for mapping the topography of an object according to claim 1 characterised in that it comprises:
 - a source for directing a beam of collimated monochromatic light along an optical axis, said optical axis extending between said source and said object;

- a beam splitter positioned on said optical axis for diverting the light rays reflected by said object off said optical axis, said reflected light having a reflected wave front having deviations from said directed wave front indicative of said topography; and
- a detector having a lens array with a plurality of lenses positioned to collectively receive said reflected wave front and individually focus the light incident on each of said lenses for mapping said topography.
3. A device for mapping the topography of an object according to claim 1 or 2 characterised in that said beam generating means comprises a laser diode and a collimating lens for collimating light emitted by said diode.
 4. A device for mapping the topography of an object according to claim 1 or 2 characterised in that said beam generating means comprises an incandescent lamp and a spectral filter, said spectral filter being positioned to pass monochromatic light from said lamp toward said object.
 5. A device for mapping the topography of an object according to any one of the preceding claims characterised in that said object is the cornea of an eye.
 6. A device for mapping the topography of an object according to any one of the preceding claims characterised in that said directed wave front of predetermined curvature is a flat wave front, and said device further comprises an objective lens for converting said flat wave front into a spherically converging wave front for incidence on said object.
 7. A device for mapping the topography of an object according to any one of the preceding claims characterised in that said object has a substantially spherical-shaped surface and objective lens is positioned for focusing said beam onto the center of curvature of said surface.
 8. A device for mapping the topography of an object according to claim 6 characterised in that it further comprises a telescopic unit for conforming said beam to fill said objective lens.
 9. A device for mapping the topography of an object according to any one of the preceding claims characterised in that said segmentally focusing means comprises a charge-coupled device and a lens array having a plurality of cylindrical lenses positioned to collectively receive said reflected wave front and individually focus the light incident on each of said cylindrical lenses onto said charge-coupled device to create a pattern on said charge-coupled device indicative of said topography.
 10. A device for mapping the topography of an object according to claim 8 characterised in that said lens array comprises a first layer having a plurality of juxtaposed cylindrical lenses and a second layer having a plurality of juxtaposed cylindrical lenses, said first layer being adjacent said second layer with said respective cylindrical lenses substantially mutually perpendicular.
 11. A device for mapping the topography of an object according to claim 8 characterised by further comprising a polarized beam splitter for directing said reflected wave front toward said lens array and a quarter wave plate, said polarized beam splitter being positioned on said beam between said objective lens and beam generating means and said quarter wave plate being positioned on said beam between said objective lens and said polarized beam splitter.
 12. A method for mapping the topography of an object characterised in that it comprises the steps of:
 - generating a beam of collimated monochromatic light characterised by having a directed wave front of predetermined curvature;
 - directing light of said beam toward said object;
 - receiving light of said beam reflected by said object, said reflected light being characterized by a reflected wave front indicative of said topography; and
 - segmentally focusing said reflected wave front to detect deviations of said reflected wave front from said directed wave front to map said topography.
 13. A method for mapping the topography of an object according to claim 12 characterised in that it further comprises the step of converting said directed wave front into a converging spherical wave front for incidence on said object.



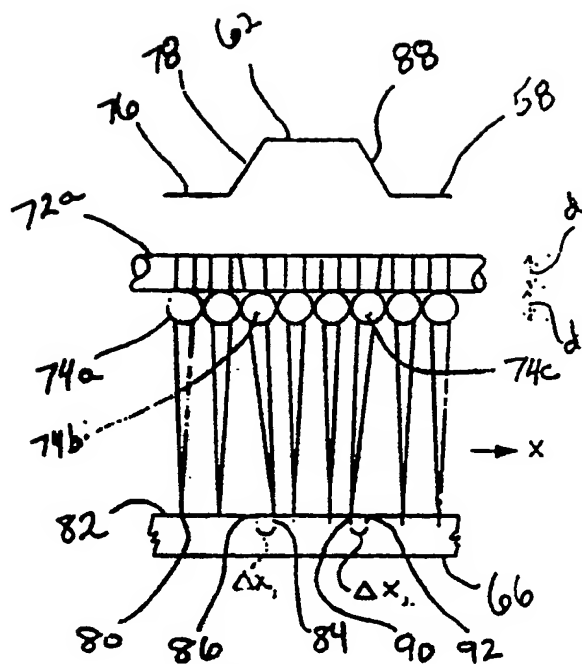


Fig. 4

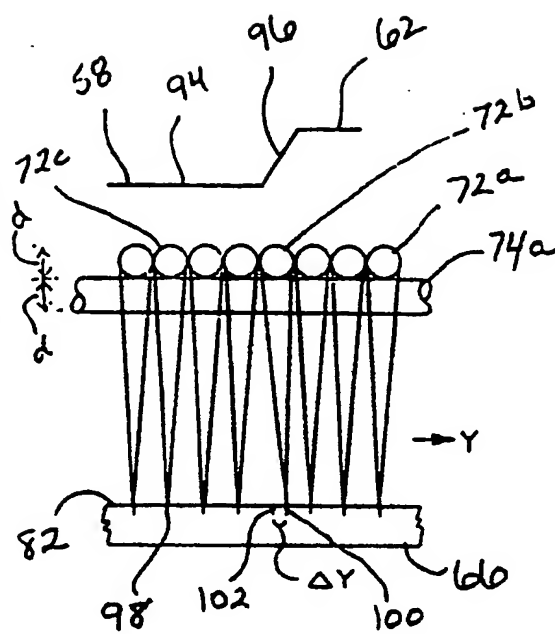


Fig. 5

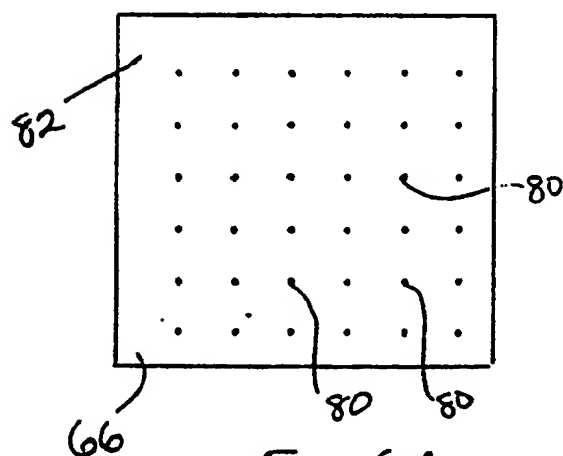


Fig. 6A

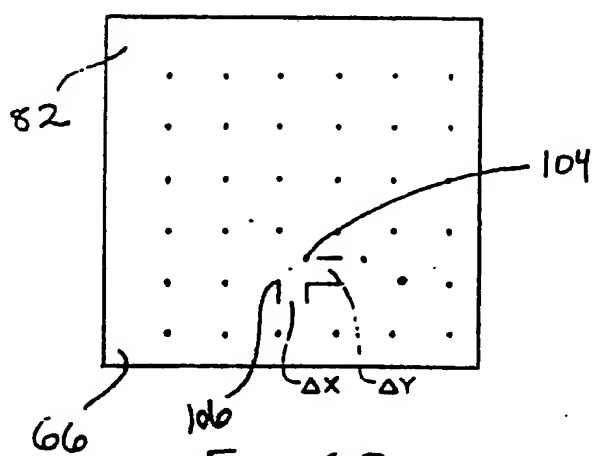


Fig. 6B



European
Patent Office

EUROPEAN SEARCH REPORT

Application Number

EP 91 30 1621

DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
X	WO-A-8 602 249 (KERASCAN, INC.) * abstract; page 5, line 2 - page 9, line 3; figure 1 *	1	A 61 B 3/107
A	-----	2-5,7,9, 12,13	
A	EP-A-0 306 409 (SYNTHELABO) * abstract; column 1, lines 1-14; column 2, line 58 - column 4, line 43; figures 1,2 *	1-3,5,8, 12	
A	----- EP-A-0 317 768 (TAUTON TECHNOLOGIES, INC.) * page 4, line 8 - page 5, line 3; figures 1,2 *	1-3,5,9, 12	
A	----- EP-A-0 317 153 (BRITISH TELECOMMUNICATIONS LTD.) * column 4, lines 14-24; figure 1 *	2,9,10	

The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			A 61 B 3/00 G 01 B 11/00 A 61 F 9/00 G 02 B 3/00
Place of search		Date of completion of search	Examiner
Berlin		19 June 91	WEIHS J.A.
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